#### ALLOWABLE STRESS DESIGN FLOWCHART

# FOR AISC MANUAL OF STEEL CONSTRUCTION, NINTH EDITION

# PART I DESIGN REQUIREMENT FOR BEAM-COLUM

SHEN-YEH CHEN, PH.D.

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S-Y. Chen, December 1997, *Using Genetic Algorithms for the Optimal Design of Structural Systems*, Dissertation for Doctor of Philosophy, Department of Civil Engineering, Arizona State University.



### DESIGN REQUIREMENET FOR BEAM-COLUMN AND OTHER FLEXURAL MEMBERS

- 0. Units: ksi (klb-in)
- 1. Applicable Range:

$$\frac{h}{t_w} \le \frac{970}{\sqrt{F_y}}$$

- 2. Allowable Stress
  - 2.1 Normal Stress: member in the structure should be proportioned to satisfied the following (Ch H1.). For details of calculating the normal allowable stress, see Appendix A.
  - (1) Bending with Axail Compression

In general

$$\begin{cases}
\frac{f_a}{F_a} + \frac{C_{mx} \cdot f_{bx}}{\left(1 - \frac{f_a}{F_{ex}}\right) \cdot F_{bx}} + \frac{C_{my} \cdot f_{by}}{\left(1 - \frac{f_a}{F_{ey}}\right) \cdot F_{by}} \le 1.0 \\
\frac{f_a}{0.6 \cdot F_y} + \frac{f_{bx}}{F_{bx}} + \frac{f_{by}}{F_{by}} \le 1.0
\end{cases}$$
(H1-1 & H1-2)

If 
$$f_a / F_a \le 0.15 \implies \frac{f_a}{F_a} + \frac{f_{bx}}{F_{bx}} + \frac{f_{by}}{F_{by}} \le 1.0$$
 (H1-3)

(2) Bending with Axial Tension

$$\frac{f_a}{F_t} + \frac{f_{bx}}{F_{bx}} + \frac{f_{by}}{F_{by}} \le 1.0 \tag{H2-1}$$

where

$$F_e = \frac{12 \cdot \pi^2 \cdot E}{23 \cdot \left(\frac{K \cdot l_b}{r_b}\right)^2}$$

 $C_m$  WITH sidesway

$$C_{m} = 0.85$$

BRACED AGAINST sidesway NO transverse loading:  $C_m = 0.6 - 0.4 \cdot \frac{M_1}{M_2}$ 

WITH transverse loading

NO rotations, both ends :  $C_m = 0.85$ WITH rotations, both ends :  $C_m = 1.0$ 

 $C_m$  can be conservatively taken as 1.0

2.2 Shear Stress:

$$\frac{f_{vx}}{F_{Vx}} + \frac{f_{vy}}{F_{Vy}} \le 1.0$$

For shear in the y direction of W and C sections

$$\frac{h}{t_w} \le \frac{380}{\sqrt{F_v}} \qquad \Rightarrow \qquad f_v = \frac{V}{\sum_i d \cdot t_w} \; ; \quad F_v = 0.4 \cdot F_y$$
 (F4-1)

$$\frac{h}{t_{yy}} > \frac{380}{\sqrt{F_{yy}}} \qquad \Rightarrow \qquad f_{y} = \frac{V}{\sum h \cdot t_{yy}} \; ; \quad F_{y} = \frac{F_{yy}}{2.98} \cdot C_{yy} \le 0.4 \cdot F_{yy}$$
 (F4-2)

All other conditions

$$\Rightarrow f_{v} = \frac{V}{\sum d \cdot t_{w}} \; ; \; F_{v} = 0.4 \cdot F_{y}$$

where 
$$\begin{pmatrix} \frac{a}{h} \le 1.0 \implies k_{v} = 4.0 + \frac{5.34}{\left(\frac{a}{h}\right)^{2}} \\ \frac{a}{h} > 1.0 \implies k_{v} = 5.34 + \frac{4.0}{\left(\frac{a}{h}\right)^{2}} \end{cases}$$
 and 
$$\begin{pmatrix} C_{v} = \frac{45000 \cdot k_{v}}{F_{v} \cdot \left(\frac{h}{f_{w}}\right)^{2}} & when \quad C_{v} \le 0.8 \\ C_{v} = \frac{190}{h} \cdot \sqrt{\frac{k_{v}}{F_{v}}} & when \quad C_{v} > 0.8 \end{pmatrix}$$

$$C_{v} = \frac{190 \cdot k_{v}}{F_{y} \cdot \left(\frac{h}{t_{w}}\right)^{2}} \quad when \quad C_{v} \leq 0.$$

$$C_{v} = \frac{190}{h_{f}} \cdot \sqrt{\frac{k_{v}}{F_{y}}} \quad when \quad C_{v} > 0.8$$

- 3. Design Requirement & Serviceability Design Consideration
  - (1) Maximum Deflection, for beams and girders supporting floors, roofs and plastered ceilings under maximum live-load

$$\frac{\Delta}{l} \le \frac{1}{360} \tag{Ch L3.1.}$$

(2) Minimum ratio of depth to length, for beams and girders in floors

$$\frac{d}{l} \ge \frac{F_y}{800} \tag{Ch C-L3.1.}$$

(3) Minimum ratio of depth to length, for roof purlins, except for flat floor

$$\frac{d}{l} \ge \frac{F_y}{1000} \tag{Ch C-L3.1.}$$

(4) Minimum ratio of depth to length, for beams supporting large floor area

$$\frac{d}{l} \ge \frac{1}{20}$$

(5) Minimum Slenderness Ratio

Design based on compressive force : 
$$\frac{Kl}{r} \le 200$$
 (Ch B7.)

Design based on tensile force : 
$$\frac{l}{r} \le 300$$
 (Ch B7.)

- 4. Stiffener See Appendix B for details.
- 5. Bearing Plate See Appendix C for details.
- 6. Cover-Plated Beam or Stiffened Beam (To be finished)

